



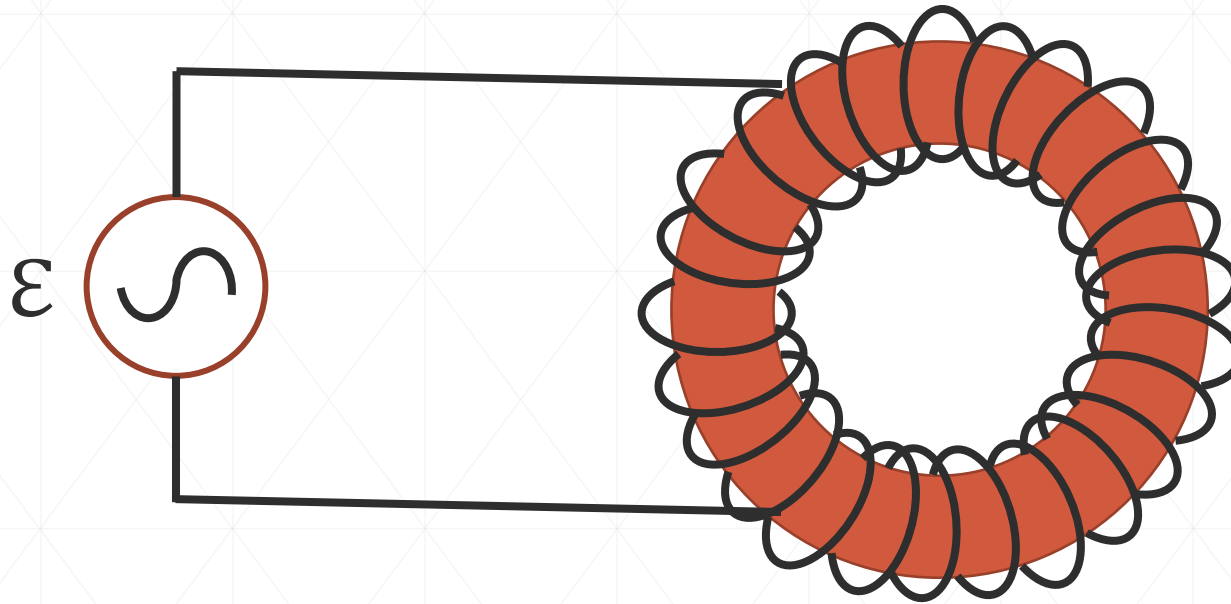
INSTITUTO DE FÍSICA

Universidade Federal Fluminense

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Eletromagnetismo

Newton Mansur



$$\mathcal{E} = Ri + \frac{d\Psi}{dt}$$

$$\mathcal{E}i = Ri^2 + i \frac{d\Psi}{dt}$$

$$\mathcal{E}idt = Ri^2dt + id\Psi$$

$$\Psi = N\phi = NBS$$

$$\mathcal{E}idt = Ri^2dt + iNSdB$$

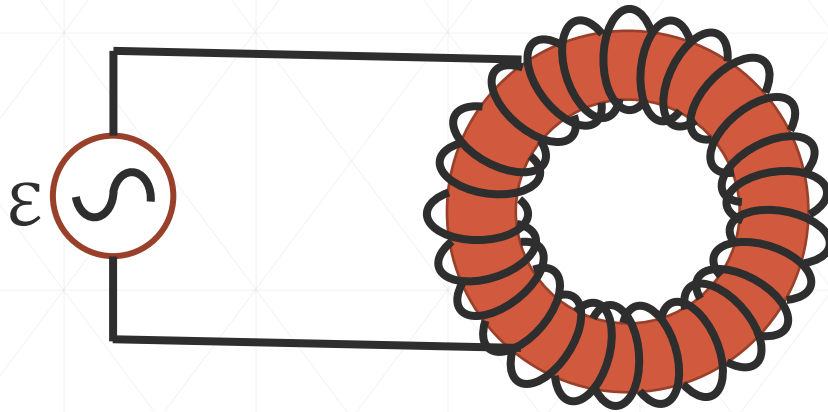
$$iNSdB \rightarrow d\left(\frac{1}{2}Li^2\right) = Lidi$$

$$H = ni = \frac{N}{l}i$$

$$Ni = Hl$$

$$dW_m = HlSdB$$

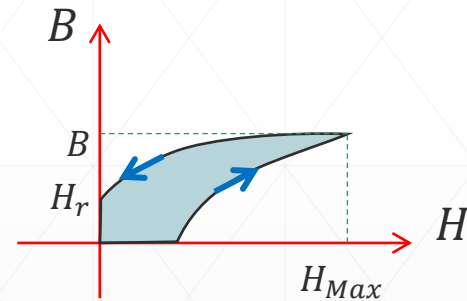
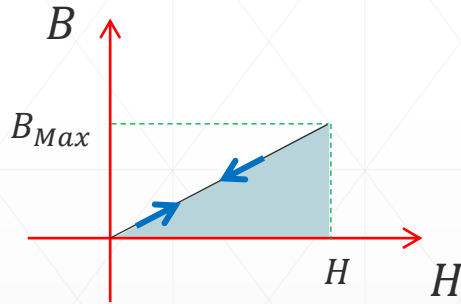
$$W_m = V \int_0^{B_{Max}} HdB$$



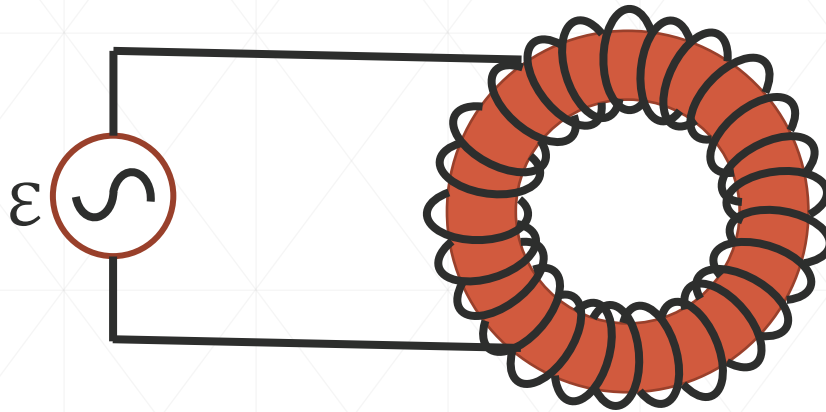
$$W_m = V \int_0^{B_{Max}} H dB$$

$$H = \mu B$$

$$W_m = \frac{1}{2} Li^2$$

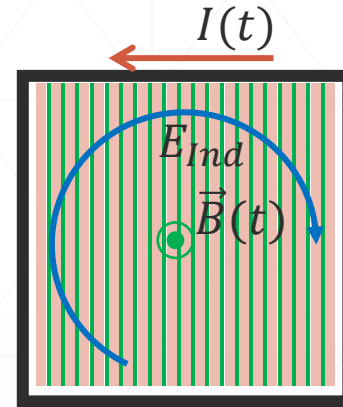
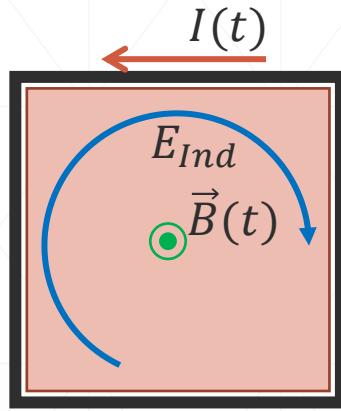


Os materiais ferromagnéticos *duros* têm ciclos de histerese com áreas grandes e dão origem a maiores perdas por histerese, não sendo adequados para a construção de máquinas eléctricas, em geral.



$$\Psi = N\phi = N \frac{NI}{R_m} = \frac{N^2}{R_m} I$$

$$L = \frac{N^2}{R_m}$$



- Materiais não duros com baixa histerese e baixa relutância
- Construído em lâminas isolados com materiais isolantes evitando corrente de Foucault

Acoplamento magnético

$$i_1 \rightarrow \phi_1 = \phi_{11} + \phi_{12}$$

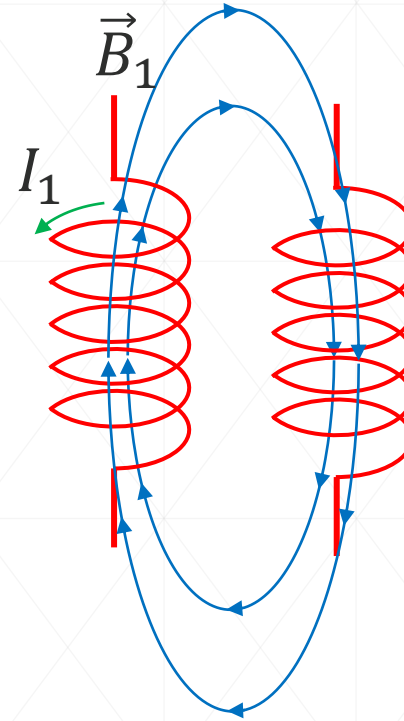
$$i_2 \rightarrow \phi_2 = \phi_{22} + \phi_{21}$$

$$\Psi_{11} = N_1(\phi_{11} + \phi_{12}) = N_1\phi_1$$

$$\Psi_{22} = N_2(\phi_{22} + \phi_{21}) = N_2\phi_2$$

$$\Psi_{1t} = N_1(\phi_1 \pm \phi_{21}) = \Psi_{11} \pm \Psi_{21}$$

$$\Psi_{2t} = N_2(\phi_2 \pm \phi_{12}) = \Psi_{22} \pm \Psi_{12}$$



$$\Psi_{1t} = L_{11}I_1 \pm M_{21}I_2$$

$$\Psi_{2t} = L_{22}I_2 \pm M_{12}I_1$$

Acoplamento magnético

$$\Psi_{1t} = L_{11}I_1 \pm M_{21}I_2$$

$$\Psi_{2t} = L_{22}I_2 \pm M_{12}I_1$$

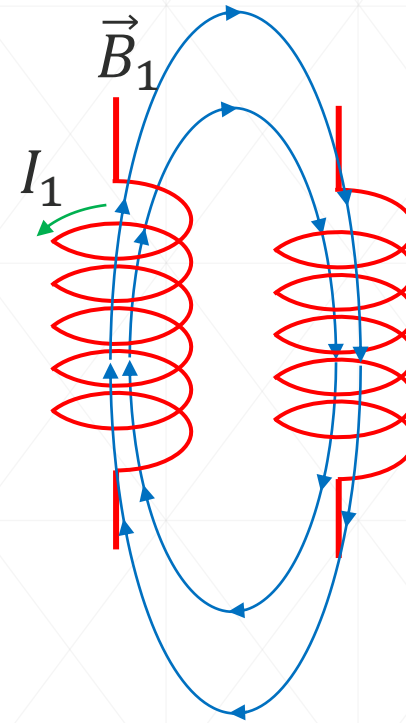
$$M_{12} = M_{21} = M$$

$$\mathcal{E}_{1t} = -\frac{d\Psi_{1t}}{dt} = -L_{11}\frac{dI_1}{dt} \mp M\frac{dI_2}{dt}$$

$$\mathcal{E}_{2t} = -\frac{d\Psi_{2t}}{dt} = -L_{22}\frac{dI_2}{dt} \mp M\frac{dI_1}{dt}$$

$$\mathcal{E}_{1t}I_1 = -\frac{d\Psi_{1t}}{dt}I_1 = -L_{11}I_1\frac{dI_1}{dt} \mp MI_1\frac{dI_2}{dt}$$

$$\mathcal{E}_{2t}I_2 = -\frac{d\Psi_{2t}}{dt}I_2 = -L_{22}I_2\frac{dI_2}{dt} \mp MI_2\frac{dI_1}{dt}$$



$$W_{mt} = \frac{1}{2}L_{11}I_1^2 + \frac{1}{2}L_{22}I_2^2 \pm M_{21}I_1I_2$$

Acoplamento magnético

$$\Psi_{1t} = L_1 I_1 + M I_2$$

$$\Psi_{2t} = L_2 I_2 + M I_1$$

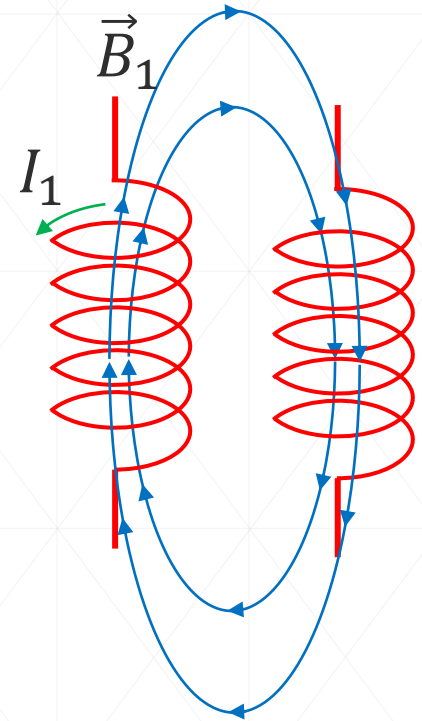
$$\begin{pmatrix} \Psi_{1t} \\ \Psi_{2t} \end{pmatrix} = \begin{bmatrix} L_1 & M \\ M & L_2 \end{bmatrix} \begin{pmatrix} I_1 \\ I_2 \end{pmatrix}$$

$$\Delta = L_1 L_2 - M^2 = L_1 L_2 \left(1 - \frac{M^2}{L_1 L_2} \right)$$

$$k = \sqrt{\frac{M^2}{L_1 L_2}} \rightarrow \text{Coeficiente de acoplamento}$$

$$M = \sqrt{L_1 L_2} \rightarrow k = 1 \text{ acoplamento ideal}$$

$$M = 0 \rightarrow k = 0 \text{ sistema desacoplado}$$



Acoplamento magnético

$$\varepsilon_1 = L_1 \frac{dI_1}{dt} + M \frac{dI_2}{dt}$$

$$\varepsilon_2 = L_2 \frac{dI_2}{dt} + M \frac{dI_1}{dt}$$

$$\varepsilon_1 = j\omega(L_1 I_1 + M I_2)$$

$$\varepsilon_2 = j\omega(L_2 I_2 + M I_1)$$

$$k^2 = \frac{M^2}{L_1 L_2}$$

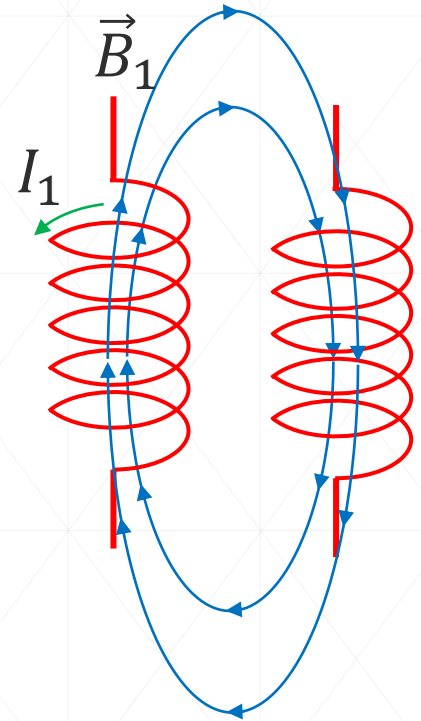
$$L_1 L_2 = \frac{M^2}{k^2}$$

$$\frac{L_1}{M} = \frac{N_1}{N_2 k}$$

$$\frac{L_2}{M} = \frac{N_2}{N_1 k}$$

$$\frac{L_1}{M} \varepsilon_2 = j\omega M \left(\frac{L_1 L_2}{M^2} I_2 + \frac{L_1}{M} I_1 \right)$$

$$\varepsilon_1 = j\omega M \left(\frac{L_1}{M} I_1 + I_2 \right)$$



Acoplamento magnético

$$\mathcal{E}_1 = \frac{L_1}{M} \mathcal{E}_2 + j\omega M \left(1 - \frac{L_1 L_2}{M^2}\right) I_2$$

$$\mathcal{E}_1 = \frac{N_1}{N_2 k} \mathcal{E}_2 + j\omega M \left(1 - \frac{1}{k^2}\right) I_2$$

$$I_1 = \frac{1}{j\omega M} \mathcal{E}_2 - \frac{N_2}{N_1 k} I_2$$

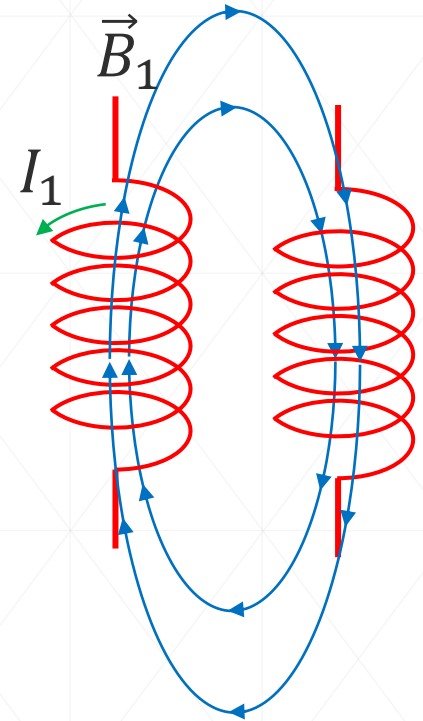
Acoplamento ideal $\rightarrow k = 1$

$$\mathcal{E}_1 = \frac{N_1}{N_2} \mathcal{E}_2$$

$$I_1 = \frac{1}{j\omega M} \mathcal{E}_2 - \frac{N_2}{N_1} I_2$$

$$\mathcal{E}_2 = 0 \rightarrow \text{Curto no secundário} \quad I_1 = -\frac{N_2}{N_1} I_2$$

$$\frac{1}{j\omega M} \mathcal{E}_2 \rightarrow \text{Corrente de magnetização}$$



Acoplamento magnético

$$\mathcal{E}_1 = j\omega(L_1 I_1 + M I_2) \quad \mathcal{E}_2 = j\omega(L_2 I_2 + M I_1)$$

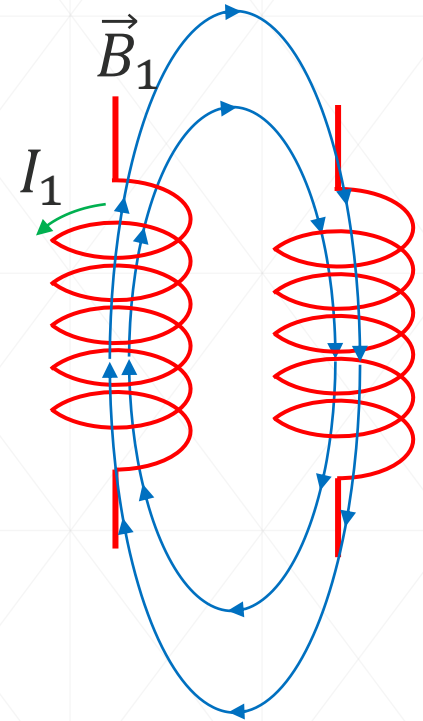
$$\mathcal{E}_1 = R_1 I_1 + j\omega(L_1 I_1 + M I_2)$$

$$\mathcal{E}_2 = R_2 I_2 + j\omega(L_2 I_2 + M I_1)$$

$$\begin{pmatrix} \mathcal{E}_1 \\ \mathcal{E}_2 \end{pmatrix} = \begin{bmatrix} R_1 & 0 \\ 0 & R_2 \end{bmatrix} \begin{pmatrix} I_1 \\ I_2 \end{pmatrix} + j\omega \begin{bmatrix} L_1 & M \\ M & L_2 \end{bmatrix} \begin{pmatrix} I_1 \\ I_2 \end{pmatrix}$$

$$\begin{pmatrix} \mathcal{E}_1 \\ \mathcal{E}_2 \end{pmatrix} = \begin{bmatrix} R_1 + j\omega L_1 & j\omega M \\ j\omega M & R_2 + j\omega L_2 \end{bmatrix} \begin{pmatrix} I_1 \\ I_2 \end{pmatrix}$$

$$\begin{pmatrix} I_1 \\ I_2 \end{pmatrix} = \begin{bmatrix} R_1 + j\omega L_1 & j\omega M \\ j\omega M & R_2 + j\omega L_2 \end{bmatrix}^{-1} \begin{pmatrix} \mathcal{E}_1 \\ \mathcal{E}_2 \end{pmatrix}$$



Equações de Maxwell

$$\nabla^2 \vec{E} = \mu_0 \epsilon_0 \frac{\partial^2 \vec{E}}{\partial t^2}$$

Em 1 dimensão

$$\frac{\partial^2 E_x(x, t)}{\partial x^2} = \mu_0 \epsilon_0 \frac{\partial^2 E_x(x, t)}{\partial t^2} = \frac{1}{v^2} \frac{\partial^2 E_x(x, t)}{\partial t^2}$$

$$v = \sqrt{\frac{1}{\mu_0 \epsilon_0}} = 2,998 \times 10^8 \frac{m}{s} = c$$

$$\frac{\partial^2 E_x(x, t)}{\partial x^2} = \frac{1}{v^2} \frac{\partial^2 E_x(x, t)}{\partial t^2}$$

$$E_x(x, t) = X(x)T(t)$$

$$\frac{1}{X} \frac{d^2 X}{dx^2} = \frac{1}{Tv^2} \frac{d^2 T}{dt^2} = -\beta^2$$

$$T(t) = T_0 e^{-j\beta vt}$$

$$X(x) = X_0 e^{\pm j\beta x}$$

$$E_x(x, t) = E_0 e^{-j\beta(\pm x + vt)}$$

$$\beta = \frac{2\pi}{\lambda}$$

$$\vec{E}(\vec{r}, t) = E_0 e^{-j(\pm \vec{\beta} \cdot \vec{r} + \omega t)}$$

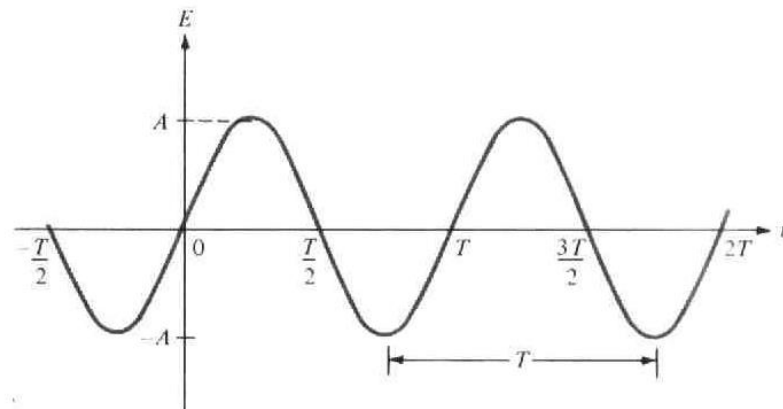
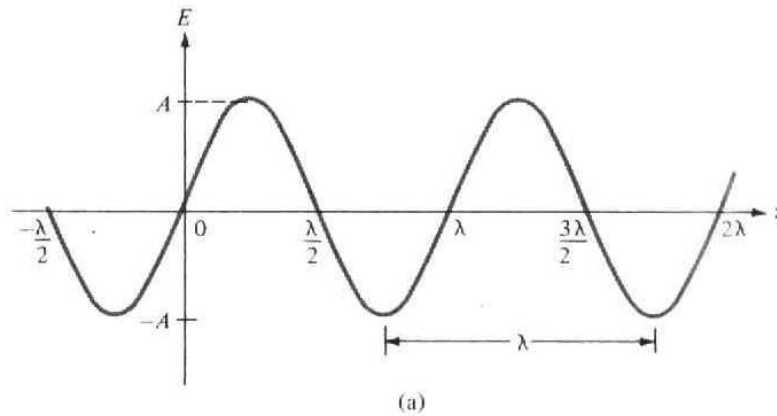
$$\beta v = \omega = \frac{2\pi}{T}$$

$$\vec{E}(\vec{r}, t) = E_0 e^{-j(\vec{k} \cdot \vec{r} \pm \omega t)}$$

$$E_x(x, t) = E_0 e^{-j(\pm\beta x + \omega t)}$$

$$\beta = \frac{2\pi}{\lambda} \quad \omega = \frac{2\pi}{T}$$

$$v = \frac{\omega}{\beta}$$



Condutor com condutividade baixa (dielétrico com perda)

$$\vec{\nabla} \cdot \vec{E} = \frac{\rho}{\epsilon_0} \quad \vec{\nabla} \cdot \vec{B} = 0$$

$$\vec{\nabla} \times \vec{H} = \vec{J} + \epsilon_0 \frac{\partial \vec{E}}{\partial t} \quad \vec{J} = \sigma \vec{E}$$

$$\vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

Sem carga livre e $\vec{E}(\vec{r}, t) = \vec{E}_0(\vec{r})e^{j\omega t}$

$$\vec{\nabla} \cdot \vec{E} = \frac{\rho}{\epsilon_0} \quad \vec{\nabla} \cdot \vec{B} = 0$$

$$\vec{\nabla} \times \vec{H} = (\sigma + j\omega\epsilon)\vec{E}$$

$$\vec{\nabla} \times \vec{E} = -j\omega\mu\vec{H}$$

Condutor com condutividade baixa (dielétrico com perda)

$$\nabla^2 \vec{E} = j\omega\mu(\sigma + j\omega\epsilon)\vec{E} \qquad \frac{\partial^2 E_x(x, t)}{\partial x^2} = j\omega\mu(\sigma + j\omega\epsilon)E_x(x, t)$$

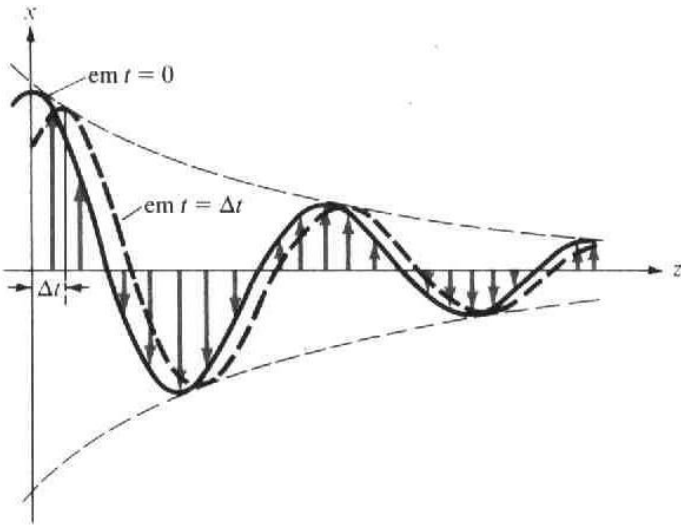
$$E_x(x, t) = E_0 e^{-j(\pm\gamma x + \omega t)}$$

$$\gamma^2 = j\omega\mu(\sigma + j\omega\epsilon)$$

$$E_x(x, t) = E_0 e^{-\alpha x} \cos(\omega t \pm \beta x)$$

$$\alpha = \omega \sqrt{\frac{\mu\epsilon}{2}} \sqrt{1 + \left(\frac{\sigma}{\omega\epsilon}\right)^2 - 1}$$

$$\beta = \omega \sqrt{\frac{\mu\epsilon}{2}} \sqrt{1 + \left(\frac{\sigma}{\omega\epsilon}\right)^2 + 1}$$



Condutor com condutividade alta (condutor quase ideal)

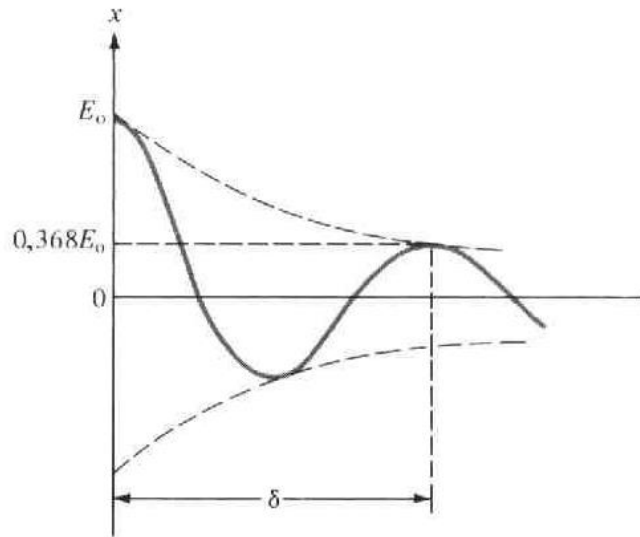
$$\alpha = \omega \sqrt{\frac{\mu\epsilon}{2} \sqrt{1 + \left(\frac{\sigma}{\omega\epsilon}\right)^2} - 1} = \sqrt{\frac{\mu\omega\sigma}{2}} \quad \beta = \omega \sqrt{\frac{\mu\epsilon}{2} \sqrt{1 + \left(\frac{\sigma}{\omega\epsilon}\right)^2} + 1} = \sqrt{\frac{\mu\omega\sigma}{2}}$$

$$E_x(x, t) = E_0 e^{-\alpha x} \cos(\omega t \pm \beta x) = E_0 e^{-x/\delta} \cos(\omega t \pm \beta x)$$

$$\delta = \sqrt{\frac{2}{\mu\omega\sigma}}$$

skin depth

Profundidade de penetração



Dielétrico sem perda

$$\sigma = 0$$

$$\alpha = \omega \sqrt{\frac{\mu\epsilon}{2} \sqrt{1 + \left(\frac{\sigma}{\omega\epsilon}\right)^2}} - 1 = 0$$

$$\beta = \omega \sqrt{\frac{\mu\epsilon}{2} \sqrt{1 + \left(\frac{\sigma}{\omega\epsilon}\right)^2}} + 1 = \omega\sqrt{\mu\epsilon}$$

Meio dispersivo

$$\beta = \omega \sqrt{\mu_0 \epsilon(\omega)}$$

$$v = \frac{\omega}{\beta} = \frac{1}{\sqrt{\mu_0 \epsilon(\omega)}}$$

